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Relocation dynamics and multistable switching in semiconductor superlattices

Guido Dell’Acqua, Luis L. Bonilla and Ramón Escobedo

*Grupo de Modelización y Simulación Numérica,
Escuela Politécnica Superior, Universidad Carlos III de Madrid,
Av. de la Universidad 30, 28911 Leganés, Madrid – Spain.
acqua@math.uc3m.es, bonilla@ing.uc3m.es, escobedo@math.uc3m.es*

Abstract

A numerical study of electric field domain relocation during slow voltage switching is presented for a spatially discrete model of doped semiconductor superlattices. The model is derived from the Poisson’s equation and the charge continuity equation. It consists of an Ampère equation for the current density and a global summatory condition for the electric field and it has been particularly effective in the prediction and reproduction of experimental results. We have designed a fast numerical scheme based on the use of an explicit expression for the current density. The scheme reproduces both previous numerical and experimental results with high accuracy, yielding new explanations of already known behaviors and new features that we present here.

*Key words: put some key words here
MSC 2000: and here the AMS codes*

1 Introduction

Semiconductor superlattices are essential ingredients in fast nanoscale oscillators, quantum cascade lasers and infrared detectors. Quantum cascade lasers are used to monitor environmental pollution in gas emissions, to analyze breath in hospitals and in many other industrial applications. A semiconductor superlattice (SL) is formed by growing a large number of periods with each period

consisting of two layers, which are semiconductors with different energy gaps but having similar lattice constants, such as GaAs and AlAs. The conduction band edge of an infinitely long ideal SL is modulated so that it looks like a one-dimensional (1D) crystal consisting of a periodic succession of a quantum well (GaAs) and a barrier (AlAs). Vertical charge transport in a SL subject to strong electric fields exhibits many interesting features, and it is realized experimentally by placing a doped SL of finite length in the central part of a diode (forming a $n^+ - n - n^+$ structure) with contacts at its ends. Depending on the bias condition, the SL configuration, the doping density, the temperature and other control parameters, the current through the SL and the electric field distribution inside the SL display a great variety of nonlinear phenomena such as pattern formation, current self-oscillations and chaotic behavior [1]. In 1998, Luo *et al.* reported experimental results on how a domain wall relocates if the voltage across the SL is suddenly changed [2]. These experiments have been explained recently by numerical simulation in a discrete model with the tunneling current density given by a constitutive relation in terms of the local electric field and the electron densities at adjacent wells [3]. Here we reproduce the model, we derive an explicit expression for the total current density which leads to an equivalent model, and we solve it with an effective numerical algorithm. We present also new features of the model which can help us to explain already known behaviors of the physical device.

2 The model

The model consists of the following Poisson and charge continuity equations:

$$F_i - F_{i-1} = \frac{e}{\varepsilon}(n_i - N_D), \quad (1)$$

$$\frac{dn_i}{dt} = J_{i-1 \rightarrow i} - J_{i \rightarrow i+1}, \quad (2)$$

for the average electric field $-F_i$ and the two-dimensional (2D) electron density n_i at the i th SL period (which starts at the right end of the $(i-1)$ th barrier and finishes at the right end of the i th barrier), with $i = 1, \dots, N$. Here N_D , ε , $-e$ and $eJ_{i \rightarrow i+1}$ are the 2D doping density at the i th well, the average permittivity, the electron charge and the tunnelling current density across the i th barrier, respectively. The SL period is $l = d + w$, where d and w are the barrier and well widths, respectively. Time-differencing Eq. (1) and inserting the result in Eq. (2), we obtain the following form of Ampere's law,

$$\frac{\varepsilon}{e} \frac{dF_i}{dt} + J_{i \rightarrow i+1} = J(t), \quad (3)$$

which may be solved with the bias condition for the applied voltage $V(t)$:

$$\frac{1}{N+1} \sum_{i=0}^N F_i = \frac{V(t)}{(N+1)l}. \quad (4)$$

The space-independent unknown function $eJ(t)$ is the total current density through the SL. We use a simplified constitutive relation for the tunneling current density across barriers in terms of the local electric field and the electron densities at adjacent wells [1]:

$$J_{0 \rightarrow 1} = \sigma F_0, \quad (5)$$

$$J_{i \rightarrow i+1} = \frac{v^{(f)}(F_i)}{l} \left\{ n_i - \frac{m^* k_B T}{\pi \hbar^2} \ln \left[1 + \exp \left(-\frac{e F_i l}{k_B T} \right) \right] \right. \\ \left. \times \left(\exp \left(\frac{\pi \hbar^2 n_{i+1}}{m^* k_B T} \right) - 1 \right) \right\}, \quad i = 1, \dots, N-1, \quad (6)$$

$$J_{N \rightarrow N+1} = \sigma F_N \frac{n_N}{N_D}. \quad (7)$$

Here σ is the contact conductivity (assumed to be the same at both contacts for simplicity), m^* the effective mass, T the temperature, k_B and \hbar are the Boltzmann and Planck constants respectively, and $v^{(f)}$ is the drift velocity:

$$v^{(f)}(F_i) = \sum_{j=1}^n \frac{\frac{\hbar^3 l (\gamma_{C_1} + \gamma_{C_j})}{2m^{*2}} \mathcal{T}_i(\mathcal{E}_{C_1})}{(\mathcal{E}_{C_1} - \mathcal{E}_{C_j} + e F_i l)^2 + (\gamma_{C_1} + \gamma_{C_j})^2}, \quad (8)$$

$$\mathcal{T}_i(\epsilon) = \frac{16 k_i^2 k_{i+1}^2 \alpha_i^2 (k_i^2 + \alpha_i^2)^{-1} (k_{i+1}^2 + \alpha_i^2)^{-1}}{(w + \alpha_{i-1}^{-1} + \alpha_i^{-1})(w + \alpha_{i+1}^{-1} + \alpha_i^{-1}) e^{2\alpha_i d}}, \quad (9)$$

$$\hbar k_i = \sqrt{2m^* \epsilon}, \quad (10)$$

$$\hbar k_{i+1} = \sqrt{2m^* [\epsilon + e(d+w)F_i]}, \quad (11)$$

$$\hbar \alpha_{i-1} = \sqrt{2m^* \left[eV_b + e \left(d + \frac{w}{2} \right) F_i - \epsilon \right]}, \quad (12)$$

$$\hbar \alpha_i = \sqrt{2m^* \left[eV_b - \frac{ewF_i}{2} - \epsilon \right]}, \quad (13)$$

$$\hbar \alpha_{i+1} = \sqrt{2m^* \left[eV_b - e \left(d + \frac{3w}{2} \right) F_i - \epsilon \right]}. \quad (14)$$

Here C_j indicates the j th subband in a well, \mathcal{E}_{C_j} is the energy level, γ_{C_j} is the scattering width, \mathcal{T}_i is the dimensionless transmission probability across the i th barrier, and eV_b is the barrier height in absence of potential drops. Typical values of these parameters are shown in Table 1.

These formulae have the advantage over pure numerical computations of being analytical and they can be used to develop the theory further. Given a known configuration of a sample used in experiments, our formulae allow calculation of constitutive relations that can be easily used to determine the dynamical behaviour of the SL.

Table 1: Parameters of the SL.

N	N_D (cm^{-2})	w/d (nm/nm)	γ (meV)	m^* (10^{-32} Kg)	\mathcal{E}_{C_1} (meV)	\mathcal{E}_{C_2} (meV)	\mathcal{E}_{C_3} (meV)	V_b (V)
40	1.5×10^{11}	9.0/4.0	8	8.43	44	180	410	0.982

For numerical treatment, it is convenient to render the equations dimensionless. We have used the following notation, introducing the typical scales of each physical magnitude:

$$F_i = F_M E_i, \quad n_i = N_D \tilde{n}_i, \quad J_{i \rightarrow i+1} = J_M \tilde{J}_{i \rightarrow i+1}, \quad J = J_M \tilde{J}, \quad (15)$$

$$v(F_i) = v_M \tilde{v}(E_i), \quad V = V_0 \phi, \quad \rho = \rho_c \tilde{\rho}, \quad x = x_0 \tilde{x}, \quad t = t_0 \tilde{t}, \quad (16)$$

The values of F_M and J_M are calculated as the coordinates of the first relative maximum of the function $J_{i \rightarrow i+1}(F_i, n_i, n_{i+1}) = J_{i \rightarrow i+1}(F_i, N_D, N_D)$. We have also defined the following dimensionless parameters

$$\nu = \frac{eN_D}{\varepsilon F_M}, \quad \rho_0 = \frac{m^* k_B T}{\pi \hbar^2 N_D}, \quad \rho_1 = e^{1/\rho_0} - 1, \quad a = \frac{e l F_M}{k_B T}, \quad (17)$$

where ν is the dimensionless doping and $\rho_0 \gg 1$ ($\rho_0 \ll 1$) denotes the high (low) temperature limit behavior of the system. The two other parameters are just for notation. The values of these parameters corresponding to the SL described in Table 1 are given in Table 2.

Table 2: Typical scales for $T = 5$ K.

F_M (kV/cm)	eJ_M (A/cm ²)	v_M (m/s)	x_0 (nm)	ν (-)	ρ_0 (-)	ρ_c (Ω m)	V_0 (V)
-	-	$\frac{J_M l}{N_D}$	$\frac{\varepsilon F_M l}{e N_D}$	$\frac{e N_D}{\varepsilon F_M}$	$\frac{m^* k_B T}{\pi \hbar^2 N_D}$	$\frac{l F_M}{e v_M N_D}$	$F_M N l$
3.945	3.127	1.691	2.494	5.212	0.111	12.62	0.205

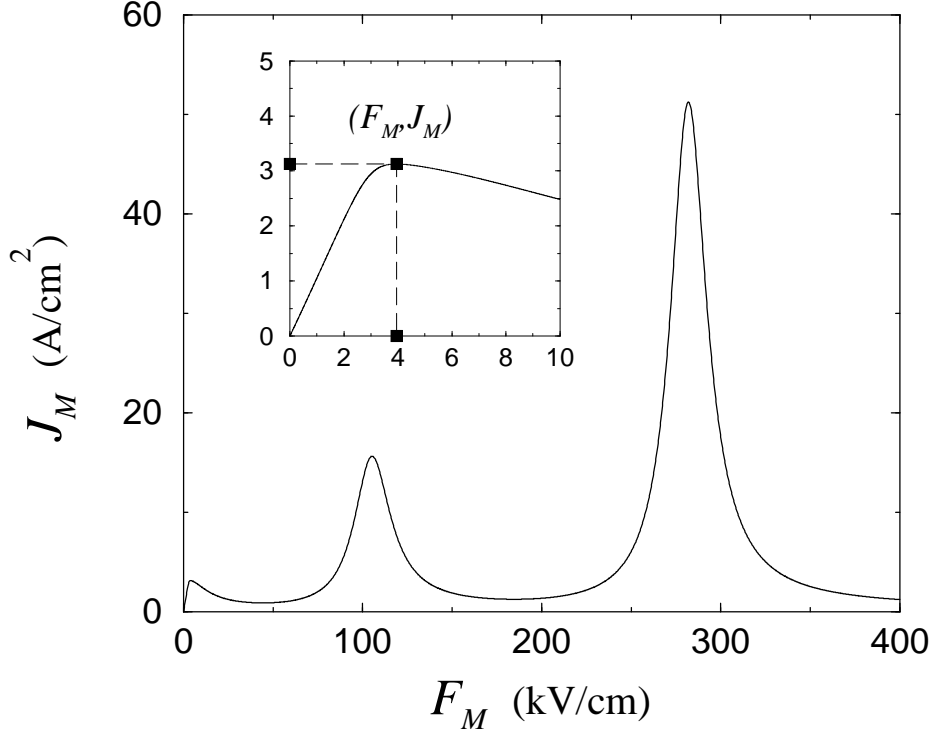


Figure 1: Constitutive relation of the tunneling current density for doping density, showing the calculation of $F_M \approx 3.945$ kV/cm and $J_M \approx 3.1269$ A/cm² for $T = 5$ K and the SL values of Table 1.

Then the dimensionless model can be written (dropping tildes) as:

$$\frac{dE_i(t)}{dt} + J_{i \rightarrow i+1}(E_i, n_i, n_{i+1}) = J(t), \quad i = 0, \dots, N, \quad (18)$$

$$n_i = \frac{E_i - E_{i-1}}{\nu} + 1, \quad i = 1, \dots, N, \quad (19)$$

$$\sum_{i=0}^N E_i(t) = (N+1)\phi(t), \quad t \geq 0, \quad (20)$$

$$J_{i \rightarrow i+1} = v(E_i) \left\{ n_i - \rho_0 \ln \left[1 + e^{-aE_i} \left(e^{\frac{n_{i+1}}{\rho_0}} - 1 \right) \right] \right\}, \quad i = 1, \dots, N-1, \quad (21)$$

$$J_{0 \rightarrow 1} = \sigma E_0, \quad (22)$$

$$J_{N \rightarrow N+1} = \sigma E_N n_N. \quad (23)$$

3 Numerical solution

The efficiency of our algorithm is based on that doing the sum in (18) from $i = 0$ to N , we obtain an explicit expression for the total current density:

$$J(t) = \frac{d\phi(t)}{dt} + \frac{1}{N+1} \sum_{i=0}^N J_{i \rightarrow i+1}(E_i(t)). \quad (24)$$

The initial system can be solved equivalently by solving, for $i = 0, \dots, N$,

$$\frac{dE_i(t)}{dt} = \frac{d\phi(t)}{dt} + \frac{1}{N+1} \sum_{j=0, j \neq i}^N J_{j \rightarrow j+1}(E_j(t)) - \frac{N}{N+1} J_{i \rightarrow i+1}(E_i(t)), \quad (25)$$

together with the initial condition $E_i(0) = \phi(0)$, $i = 0, \dots, N$. Note that the bias condition is preserved: summing again in (25) yields

$$\frac{d}{dt} \left[\sum_{i=0}^N E_i - (N+1)\phi \right] = \frac{1}{N+1} \sum_{i=0}^N \left(\sum_{j=0, j \neq i}^N J_{j \rightarrow j+1} \right) - \frac{N}{N+1} \sum_{i=0}^N E_i, \quad (26)$$

which is equal to zero, so $\sum_{i=0}^N E_i(t) = (N+1)\phi(t)$ plus a constant, which may be zero to fulfill the initial condition.

We have used explicit and implicit methods to solve this system: an order one Euler method, an embedded Runge-Kutta method of order 7(8) with step-size control and error estimate, and BDF methods of order 1 to 4. Implicit methods are solved by means of Newton-Raphson iterations.

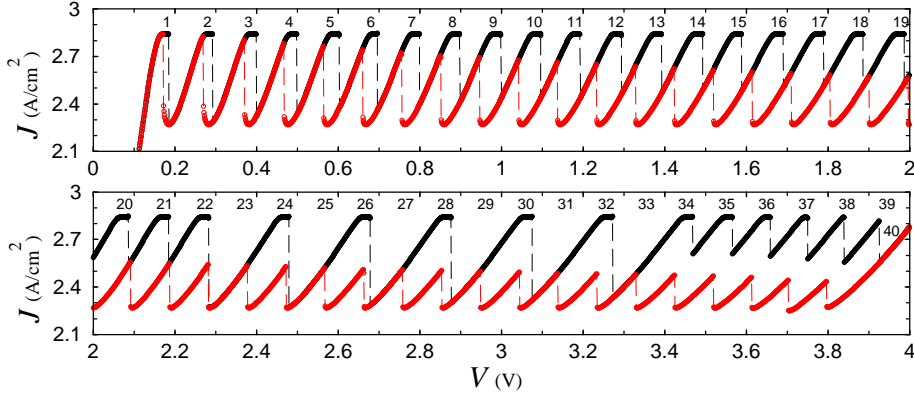


Figure 2: Current-voltage diagram for $T = 5$ K and $\rho = 25.2 \Omega\text{m}$ showing stationary branches B_i , $i = 1, \dots, N$, and regions of multistability.

Results. Fig. 2 shows the current-voltage characteristic curve for the SL values of Table 1 and 2. For constant ϕ , the stable field profiles $\{E_i\}$ are time-independent, step-like and increasing with i : typically they consist of two flat regions called electric field domains separated by an abrupt transition region called a domain wall or charge monopole [1].

The electric field profiles of each branch of solutions in Fig. 2 differ in the location of their domain wall: counting branches in the direction of increasing voltage, the profiles of the j th branch have their domain wall located in the $(N - j + 1)$ th SL period. Notice that for certain values of the voltage, several branches with different current are possible (multistability). The central part of the first branches (from B_1 to B_{21} in Fig. 2) are regions of monostability. The upper and lower limits of these branches overlap with the previous and the following ones, defining intervals of bistability. The 22th branch is the last having a region of monostability and the first whose upper limit overlaps with the two following branches, describing a region of tristability. Branches B_{22} to B_{39} are all bistable/tristable, and the last branch B_{40} has the three types of behavior: it is tristable in the lower limit, bistable in the central part, and monostable in the upper limit.

If we switch the voltage from a value V_{ini} corresponding to one branch to a final value $V_{\text{end}} = V_{\text{ini}} + \Delta V$ corresponding to different branches, the domain wall has to relocate in a different SL period. During switching, $V(t) = V_{\text{ini}} + \dot{V}t$, with $\dot{V} = \Delta V/\Delta t$, and Δt is the ramping time.

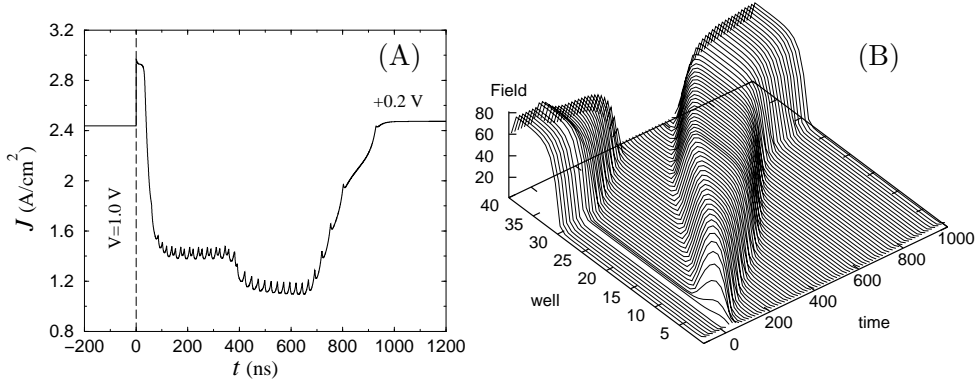


Figure 3: Relocation of the electric field wall for $T = 5$ K and $\rho = 25.2 \Omega\text{m}$. For $t < 0$, $V = 1.0$ V in B_{10} . At $t = 0$, we add $\Delta V = 0.2$ V and reach B_{12} . (A) Current density during relocation: $J(t)$ starts at 2.44 A/cm², then falls to low values at $t \approx 20$ ns, it describes the double/single peaks pattern observed in the experiments, and finally grows again to a stationary value of 2.47 A/cm². (B) Electric field, showing the domain relocation from well 31 to well 29.

Fig. 3 shows the current density and the electric field evolution during a relocation with $\Delta t = 0$. In this case, the current density exhibits an interval of double peaks, followed by an interval of single peaks, between both stationary states, accompanied in the electric field distribution by the nucleation of a dipole wave at the injecting contact, which crosses the sample and is finally absorbed by the high field domain. See Fig. 3(B). All these features are as observed in the experiments [2, 3, 4].

For larger values of ΔV , this scenario is repeated a number of times equal to the number of branches crossed in ΔV , provided Δt is greater than a critical value t_c . Fig. 4 shows that depending on if Δt is greater than t_c or not, the curve $(V(t), J(t))$ has time or not to describe the same number of pics than branches the voltage crosses.

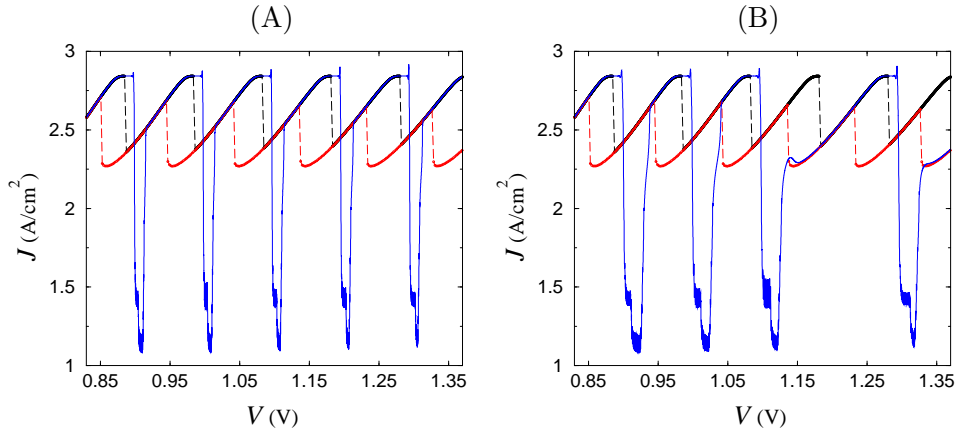


Figure 4: Current density curve $(V(t), J(t))$ (solid line) during the voltage switching from $V_{\text{ini}} = 0.83$ V to $V_{\text{end}} = 1.37$ V for a large ramping time and the half: (A) $t_{\text{ramp}} = 30 \mu\text{s}$ and (B) $t_{\text{ramp}} = 15 \mu\text{s}$. Also depicted (small circles) are the stationary branches of the I - V characteristic of Fig. 2.

The system evolves with $\phi(t)$ near a stationary branch until the upper limit is reached; then it falls to the next branch. This change of branch is produced by means of the relocation of the electric field domain by injecting a dipole wave at the cathode. During this process, the current decreases to low values to allow the emission and the trip of the dipole wave. Once the wave is absorbed by the high field domain, the current returns to a stationary value located in the next branch. See Fig. 4 (A) for $\Delta t = 30 \mu\text{s}$ and (B) for $\Delta t = 15 \mu\text{s}$. Voltage values are $V_{\text{ini}} = 0.83$ V and $V_{\text{end}} = 1.37$ V.

Two different behaviors are observed:

- When $\Delta t > t_c$, the return of the current density to the I - V branch takes place in a region of monostability, allowing the curve to follow the branch

again, until the upper limit is reached. This is repeated 4 times, and it is accompanied with the corresponding five emissions of a dipole wave. Fig. 5(A) shows one of these five relocation processes by injection of a wave corresponding to Fig. 4(A).

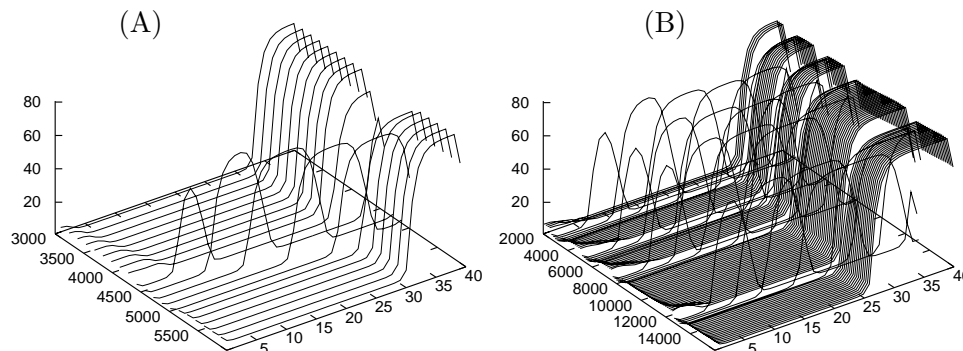


Figure 5: Electric field distributions during voltage switching for both ramping times shown in Fig. 4. (A) Example of domain relocation by means of the absorption of the electric dipole wave. (B) Switching process for $t_{\text{ramp}} = 15\mu\text{s}$, showing the absence of the 4th and 6th waves.

- When $\Delta t < t_c$, the curve $(V(t), J(t))$ returns to a range of bistability and falls to the lower branch. Fig. 4(B) shows that after having been following the third branch, the curve falls to low values of J to allow the injection of a dipole wave, as before. However, when it returns to stationary values, the curve has not time to reach the 4th branch before entering into the bistability region of branches 4 and 5. Then the curve goes to the 5th branch, and the 4th branch has been dropped. The result is that the current density curve exhibits one maximum less, and the electric field has injected only four dipole waves during this shorter switching time. The same thing occurs with the 6th branch, which is also dropped; see again Fig. 4(B).

In conclusion, we have presented a new formulation of a domain relocation problem and the numerical simulations which gives a more satisfactory explanations of a previously observed behavior of the device, in terms of the stability intervals of the applied voltage. These results have been obtained with a fast and effective numerical algorithm based on this new formulation.

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