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# Wave fronts, pulses and wave trains in photoexcited superlattices behaving as excitable or oscillatory media

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## Abstract

Undoped and strongly photoexcited semiconductor superlattices with field-dependent recombination behave as excitable or oscillatory media with spatially discrete nonlinear convection and diffusion. Infinitely long, dc-current-biased superlattices behaving as excitable media exhibit wave fronts with increasing or decreasing profiles, whose velocities can be calculated by means of asymptotic methods. These superlattices can also support pulses of the electric field. Pulses moving downstream with the flux of electrons can be constructed from their component wave fronts, whereas pulses advancing upstream do so slowly and experience saltatory motion: they change slowly in long intervals of time separated by fast transitions during which the pulses jump to the previous superlattice period. Photoexcited superlattices can also behave as oscillatory media and exhibit wave trains.

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(Some figures in this article are in colour only in the electronic version)

## 1. Introduction

Vertical nonlinear charge transport in undoped, weakly coupled, photoexcited superlattices (SLs) has many similarities to extended excitable or oscillatory media. In both cases, traveling waves such as wave fronts, pulses or wave trains play an important role in the dynamics of the system [1]. In undoped SLs, the formation and dynamics of electric field domains (EFDs) are the basic mechanisms behind more complex phenomena such as self-sustained oscillations of the current (SSOC) through voltage-biased SLs, chaos, etc. Interfaces separating EFDs are wave fronts or wave front-bound pulses, and pulses are the building blocks of wave trains. While there are at least two stable EFDs with an almost constant value of the electric field in the case of doped SLs, there may be only one stable EFD in the case of an undoped SL

under high photoexcitation [2]. This is similar to what happens in excitable media such as those described by the FitzHugh–Nagumo (FHN) model for nerve conduction [3, 4]. For background information on this model and related models, see [5–11, 1]. The case of an oscillatory medium in which there is a single unstable spatially homogeneous state can also be realized in both the FHN model and a strongly photoexcited undoped SL [2]. However, the electric field in a voltage-biased SL with a finite number of periods is constrained to have a fixed area underneath its spatial profile, and this constraint causes it to exhibit a more complex behavior [2].

The key ingredient to the complex dynamics of electron transport in photoexcited undoped SLs is the introduction of an electron–hole recombination coefficient, which is a function of the electric field. Nonlinear charge transport in weakly coupled undoped type-I SLs under photoexcitation is well described by spatially discrete drift-diffusion systems (DDDS) of equations [12–14]. In earlier models, the electron–hole recombination was considered to be a constant, independent of the electric field [12]. In this case, there are three stable states with spatially homogeneous field profiles, and the predicted nonlinear phenomena are then quite similar to the ones observed in the much better known case of doped SLs (in which the hole density is replaced by a constant doping density): the dynamics is organized by stable wave fronts that join the stable homogeneous states [14]. Introducing a field-dependent electron–hole recombination coefficient in the model has striking consequences [2]. For high photoexcitation densities, it is possible to find only one stable EFD, not two as in the case of a constant recombination coefficient [12]. Then, under a dc voltage bias, periodic or chaotic SSOC may appear. The field profile during self-oscillations may exhibit nucleation of dipole waves inside the sample, splitting of one wave in two, and motion of the resulting waves in opposite directions. Despite the strong asymmetry induced by the drift terms in the equations, these dipole waves resemble the pulses in the FHN model for nerve conduction [9, 11] and are quite different from field profiles for a field-independent recombination coefficient [12].

In this paper, we construct relevant stable solutions of the DDDS of equations for dc-current-biased SL by means of asymptotic and numerical methods that extend and refine those used for the discrete FHN system [15, 16]. For an undoped SL that acts as an excitable medium (only one stable EFD), we find that electric field pulses moving downstream with the electron flux can be described using matched asymptotic expansions based on separating the sharp leading and trailing wave fronts of the pulse from smoother regions outside them. Pulses moving upstream do so much more slowly and experience a saltatory motion, in which intervals of a slow change are separated by fast changes during which the pulse jumps to the previous SL period. For an undoped SL acting as an oscillatory medium (a single unstable EFD), we construct periodic wave trains consisting of an infinite succession of pulses.

## 2. Model equations

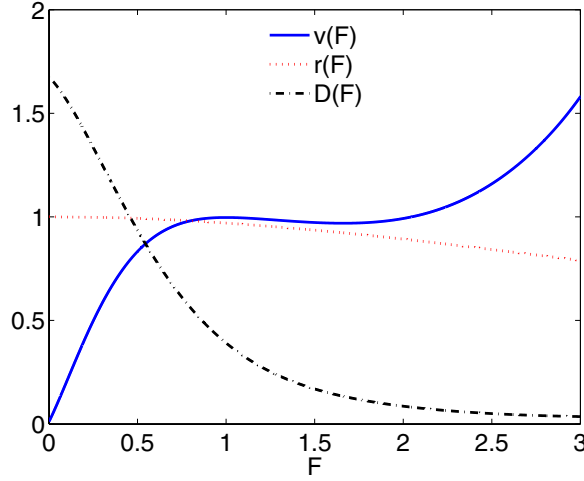
Written in nondimensional form, the equations governing nonlinear charge transport in a weakly coupled, undoped, photoexcited GaAs/Al<sub>x</sub>Ga<sub>1-x</sub>As SL are [2]

$$F_i - F_{i-1} = v(n_i - p_i), \quad (1)$$

$$\delta \frac{dF_i}{dt} + n_i v(F_i) - D(F_i)(n_{i+1} - n_i) = J, \quad (2)$$

$$\frac{dp_i}{dt} = 1 - r(F_i) n_i p_i, \quad (3)$$

where  $i$  takes on integer values corresponding to the spatial periods of the SL.  $F_i$ ,  $n_i$  and  $p_i$  are the average electric field, electron and hole surface densities at the  $i$ th SL period,



**Figure 1.** Electron velocity  $v$ , diffusion coefficient  $D$ , and recombination coefficient  $r$  versus electric field  $F$  for a GaAs/Al<sub>0.3</sub>Ga<sub>0.7</sub>As SL with a well width  $L_W = 10$  nm and barrier width  $L_B = 4$  nm. The lattice temperature is assumed to be 200 K.

respectively, and the dimensionless parameters  $v$ ,  $\delta$  and  $r$  are described below. Equation (1) refers to the averaged Poisson equation, while equation (2) corresponds to Ampère’s law: the total current density  $J$  equals the sum of the displacement current density  $\delta \, dF_i/dt$  and the electron tunneling current density across the  $i$ th barrier that separates wells  $i$  and  $i + 1$ , i.e.  $J_{i \rightarrow i+1} = n_i v(F_i) - D(F_i)(n_{i+1} - n_i)$ . Note that the tunneling current density has a discrete drift term with electron velocity  $v(F)$  and a diffusive term with diffusion coefficient  $D(F)$ . Charge continuity is obtained by differentiating equation (1) with respect to time and using equation (2) in the result

$$v\delta \frac{d}{dt}(n_i - p_i) + J_{i \rightarrow i+1} - J_{i-1 \rightarrow i} = 0. \tag{4}$$

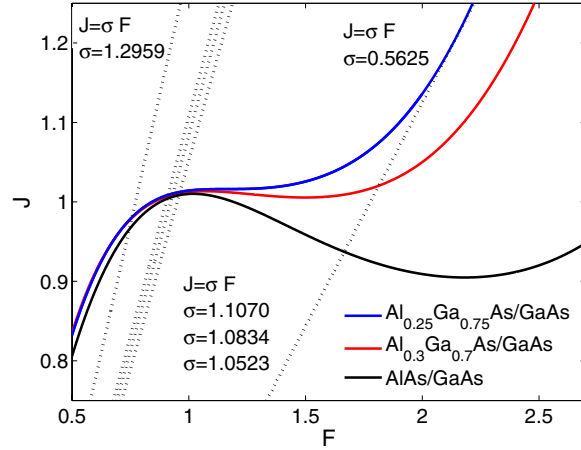
Tunneling of holes is neglected so that only photogeneration and recombination with electrons enter equation (3). The field-dependent quantities  $v$ ,  $D$ , and the recombination coefficient  $r$  are described in [2] and their field dependences are depicted in figure 1. The dimensionless parameter  $v$  is a ratio between the carrier density scale determined by photogeneration and recombination and the carrier density determined by scattering processes. The dimensionless parameter  $\delta$  is the ratio between the time scales of dielectric relaxation and recombination [2]. These parameters depend on the photoexcitation density and the Al content  $x \in (0, 1]$  in the SL barriers. For high photoexcitation densities,  $\delta \ll 1$ , whereas  $\delta \gg 1$  for small photoexcitation densities. The parameter  $v$  can be of any order.

It is interesting to depict the phase plane corresponding to spatially uniform solutions of equations (1)–(3) with  $n_i = p_i = p$ ,  $F_i = F$ :

$$\delta \frac{dF}{dt} = J - pv(F), \quad \text{and} \quad \frac{dp}{dt} = 1 - r(F) p^2. \tag{5}$$

Generically and for fixed  $J$ , the nullclines  $v(F) p = J$  and  $r(F) p^2 = 1$  intersect in one or three fixed points, depending on the Al content  $x$  in the barriers, a parameter that controls the functions  $v(F)$ ,  $D(F)$  and  $r(F)$  [2]. At these fixed points,

$$j(F) = J, \quad j(F) = \frac{v(F)}{\sqrt{r(F)}}. \tag{6}$$



**Figure 2.** Local current density  $j$  versus electric field  $F$ . For a fixed value of the total current density  $J$ , there may be one or three zeros of  $j(F) - J$  depending on the Al content  $x$ . The dashed lines are the boundary condition  $J = \sigma F$  for the different values of the dimensionless contact conductivity  $\sigma$  indicated in the figure.

The function  $j(F)$  is depicted in figure 2. For  $0.45 \leq x \leq 1$ , there are three fixed points of the system in equation (5), one on each of the three branches of  $p = J/v(F)$ , and the ratio between  $j_{\max} - j_{\min}$  and the average current  $(j_{\max} + j_{\min})/2$  is sufficiently large. In this case, nonlinear phenomena are quite similar to those observed in doped SL: static electric field domains with domain walls joining the stable branches of  $p = J/v(F)$ , SSOC in voltage-biased SL due to the recycling of pulses formed by two moving domain walls bounding a high field region, etc. For  $0 < x < 0.45$ ,  $j(F)$  is either increasing for positive  $F$  (if  $0 < x < 0.25$ ) or the ratio  $2(j_{\max} - j_{\min})/(j_{\max} + j_{\min})$  is small (if  $0.25 < x < 0.45$ ). For  $0 < x < 0.25$ , there is a unique fixed point at  $F = F_*$ , which for an appropriate value of  $J$  may be located at any of the three branches of  $p = J/v(F)$ . If the fixed point is located at one of the two stable branches of  $p = J/v(F)$  for which  $v(F)$  has a positive slope, the dynamical system of equation (5) is excitable, whereas it is oscillatory if the fixed point is located on the second branch of  $v(F)$  with negative slope. We will see later that quite unusual phenomena are found for these cases. Under dc current bias, it is possible to have pulses moving to the right or to the left and periodic wave trains. Under dc voltage bias, these pulses and wave trains may give rise to SSOC [2].

### 3. Wave fronts in a dc-current-biased photoexcited SL behaving as an excitable medium

Wave fronts and pulses of the electric field and carrier densities are key elements in the description of stable solutions of our model equations. We will start by describing these solutions for an infinite SL under a constant current bias  $J$  in the limit of high photoexcitation densities,  $\delta \ll 1$ , in which the dynamical behavior of the SL is richer [2]. In this section, we focus our attention on wave fronts, while we will deal with pulses in the next section.

#### 3.1. Leading order construction of wave fronts

A wave front is a moving interface separating regions of smooth field variation on the time scale  $t$ . Inside the front,  $F_i$  varies rapidly on the time scale  $t/\delta$ . Let us eliminate the electron

density  $n_i$  by using equation (1) in equations (2)–(3):

$$\delta \frac{dF_i}{dt} + v(F_i) \frac{F_i - F_{i-1}}{v} - D(F_i) \frac{F_{i+1} + F_{i-1} - 2F_i}{v} = J - v(F_i)p_i + D(F_i)(p_{i+1} - p_i), \quad (7)$$

$$\frac{dp_i}{dt} = 1 - r(F_i) p_i \left( p_i + \frac{F_i - F_{i-1}}{v} \right), \quad (8)$$

In the regions where the field varies smoothly, we can set  $\delta = 0$ ,  $F_i = F_{i-1}$ ,  $n_i = p_i$  in equations (7)–(8), thereby obtaining the reduced problem

$$p_i v(F_i) = J, \quad (9)$$

$$\frac{dp_i}{dt} = 1 - r(F_i) p_i^2. \quad (10)$$

In the wave fronts that separate these regions, the electric field and the hole density vary rapidly as  $F_i(t) = F(\xi)$ ,  $p_i(t) = p(\xi)$ , with  $\xi = i - ct/\delta$ . In these regions, equations (7) and (8) yield to leading order

$$\begin{aligned} -c \frac{dF}{d\xi} = J - \left[ p + \frac{F(\xi) - F(\xi - 1)}{v} \right] v(F(\xi)) \\ + D(F(\xi)) \frac{F(\xi + 1) + F(\xi - 1) - 2F(\xi)}{v}, \end{aligned} \quad (11)$$

$$-c \frac{dp}{d\xi} = 0. \quad (12)$$

Thus,  $p$  is a constant equal to the value  $p_i(t)$  at the last point in the region of smooth variation before the front. Let  $F^{(1)}(p) < F^{(2)}(p) < F^{(3)}(p)$  be the solutions of  $J/v(F) = p$  for  $v_{\min} < J/p < v_{\max}$ , where the local maximum and minimum of the velocity  $v(F)$  are reached at  $(F_{\max}, v_{\max})$  and at  $(F_{\min}, v_{\min})$ , respectively (with  $F_{\max} < F_{\min}$ ). Let us assume that the front velocity is positive,  $c > 0$ . Equation (11) has *decreasing* front solutions (DFs) such that the profile  $F(i - ct/\delta)$  is a decreasing function satisfying the boundary conditions

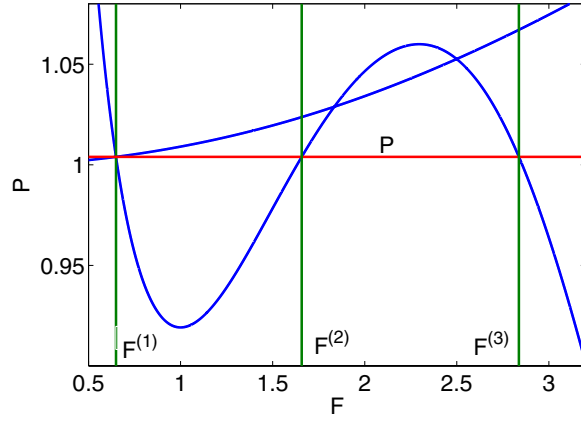
$$F(-\infty) = F_i(+\infty) = F^{(3)}(p), \quad F(+\infty) = F_i(-\infty) = F^{(1)}(p), \quad (13)$$

and *increasing* front solutions (IFs) with an increasing profile  $F(i - ct/\delta)$  that satisfies the boundary conditions

$$F(-\infty) = F_i(+\infty) = F^{(1)}(p), \quad F(+\infty) = F_i(-\infty) = F^{(3)}(p). \quad (14)$$

In figure 3, we show the nullclines  $p = J/v(F)$  and  $p = [r(F)]^{-1/2}$  for fixed  $J$  corresponding to equation (5) in a GaAs/AlAs SL. Depending on the parameters, the increasing function  $p = [r(F)]^{-1/2}$  may intersect the cubic  $p = J/v(F)$  in one, two or three critical points. At least one critical point on the first or third branch of  $p = J/v(F)$  makes our system behave as an excitable medium, whereas if there is only one critical point on the second branch of  $p = J/v(F)$ , our system has an oscillatory character, as we will see later. In figure 3, we have also shown a horizontal line for a given constant value of  $p$ , which joins the first and third branches of  $p = J/v(F)$ . This line corresponds to a wave front with fixed  $p$  as explained above.

For sufficiently large  $v$ , there are two critical values of the current density,  $J_{c1}$  and  $J_{c2}$ , so that IFs move to the right ( $c > 0$ ) if  $J < J_{c1}$ , are pinned ( $c = 0$ ) if  $J_{c1} < J < J_{c2}$  and move to the left ( $c < 0$ ) if  $J > J_{c2}$ , as shown in figure 4(a). A similar picture holds



**Figure 3.**  $p$ - $F$  phase plane exhibiting nullclines for fixed  $J$  and a wave front at constant  $p$  in a GaAs/AlAs SL.

for DFs (cf figure 4(b)). Near the critical currents  $J_{ci}$  ( $i = 1, 2$ ), the wavefront profiles and their velocities can be approximately found by means of the theory of active quantum wells (QWs) developed for doped SLs in [17] (the only change is replacing  $J/p$  and  $v/p$  instead of  $J$  and  $v$  in the expressions for doped SLs). In the limit  $v \rightarrow 0+$ , the equations for the fronts can be approximated by their continuum limit, which is a first-order hyperbolic partial differential equation having shock waves among its solutions, and the shock velocity gives a good approximation of the wavefront velocity [17].

The theory we have just sketched holds in the limit as  $\delta \rightarrow 0$ , and we would expect that it also holds for sufficiently small positive values of  $\delta$ . However, a comparison of the front velocity given by the asymptotic theory with the one obtained by direct numerical simulation shows a remarkable difference even for quite small values of  $\delta$ . The difference between the approximate and numerical velocities for  $\delta = 0.018$  is about 0.06, which gives a relative error of 25%. This error is reduced to 2% for  $\delta = 0.001$ . Nevertheless, we would like to have an asymptotic theory, which is better than this. How do we correct the simple wavefront construction given above?

### 3.2. Corrected asymptotic theory of wave fronts

To correct the previous leading order theory of wave fronts, we use the fact that the DF or IF profiles are monotone functions of a variable  $\xi = i - ct/\delta$ . Thus,

$$F_i(t) = \mathcal{F}(\xi), \quad p_i(t) = \mathcal{P}(\xi), \tag{15}$$

with  $\mathcal{F}'(\xi) < 0$  (respectively  $> 0$ ) for DF (respectively IF). In either case, we can find

$$\xi = \Xi(F) \quad \text{which solves} \quad \mathcal{F}(\xi) = F. \tag{16}$$

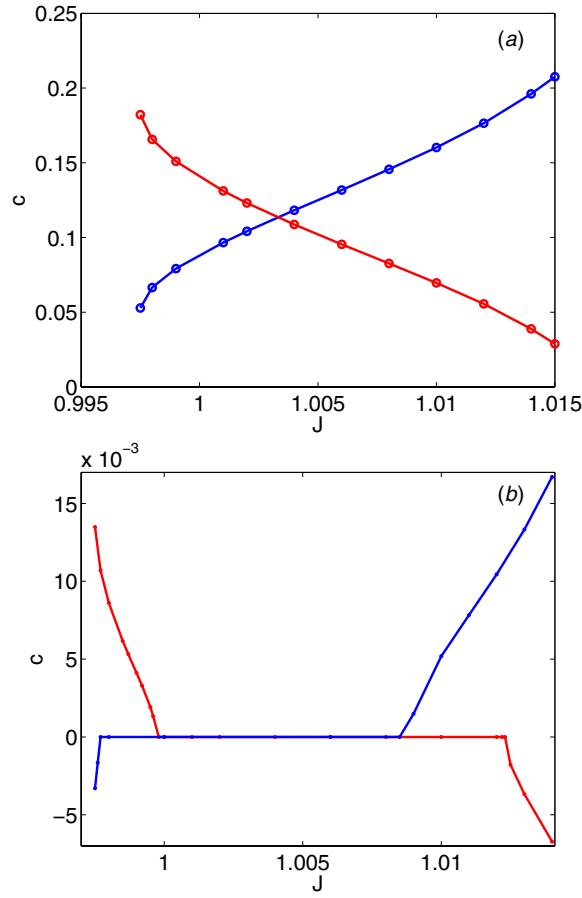
Then, the finite differences

$$F_i - F_{i-1} = \mathcal{F}(\xi) - \mathcal{F}(\xi - 1) = F_i - \mathcal{F}(\Xi(F_i) - 1), \quad \text{and} \tag{17}$$

$$F_{i+1} + F_{i-1} - 2F_i = \mathcal{F}(\Xi(F_i) + 1) + \mathcal{F}(\Xi(F_i) - 1) - 2F_i$$

can be considered to be functions of  $F_i$ . Therefore, we can derive from the equation for  $p_i(\xi)$

$$-c \frac{dp_i}{d\xi} = \delta \left[ 1 - r(F_i) p_i \left( p_i + \frac{F_i - F_{i-1}}{v} \right) \right] \tag{18}$$



**Figure 4.** Dimensionless velocities of DF and IF as a function of the dimensionless current density  $J$  for (a)  $v = 8.45$  and (b)  $v = 330$  with  $x = 0.25$  and  $p$  fixed. The DF (respectively IF) velocity increases (respectively decreases) with increasing  $J$ .

and from the equation for the wavefront field profile the following equation for  $p_i$  as a function of the field  $F_i$ :

$$\frac{dp_i}{dF_i} = \frac{\delta}{J} \frac{1 - r(F_i) p_i \left( p_i + \frac{F_i - F_{i-1}}{v} \right)}{1 - \left( p_i + \frac{F_i - F_{i-1}}{v} \right) \frac{v(F_i)}{J} + \frac{D(F_i)}{J} \left( p_{i+1} - p_i + \frac{F_{i+1} + F_{i-1} - 2F_i}{v} \right)}. \quad (19)$$

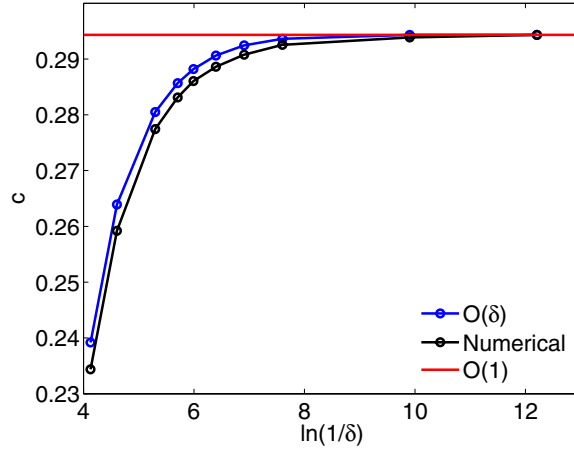
Now we integrate this equation and iterate the result starting from the value  $p_i(F_0) = p$ , thereby obtaining

$$p_i \sim p + \frac{\delta}{J} \int_{F_0}^{F_i} \frac{\left[ 1 - r(F) p \left( p + \frac{F - \mathcal{F}(\Xi(F) - 1)}{v} \right) \right] dF}{1 - \left( p + \frac{F - \mathcal{F}(\Xi(F) - 1)}{v} \right) \frac{v(F)}{J} + \frac{D(F)}{J} \left( \frac{\mathcal{F}(\Xi(F) + 1) + \mathcal{F}(\Xi(F) - 1) - 2F}{v} \right)} \quad (20)$$

up to terms of order  $\delta^2$ .

The starting point  $F_0$  should be selected so as to ensure convergence of the integral in equation (20). If  $p = p_*$  corresponds exactly to a critical point, we can select  $F_0$  as the field value of the same critical point  $F_*$ . Then, the integrand has a finite limit as  $F \rightarrow F_0$ , and the integral in equation (20) converges. If this is not the case, we need a nonzero value of the finite





**Figure 5.** Comparison of the numerically obtained and asymptotic approximations for the DF velocity as a function of  $\ln(1/\delta)$  using the parameter values  $x = 0.3$ ,  $J = 1.006$ , and  $v = 4.449$ .

difference  $F_0 - \mathcal{F}(\Xi(F_0) - 1)$  to obtain a nonzero value of the denominator in equation (19). We use the slow scale equation (9) to calculate  $F_i = \Phi(p_i)$ . Inserting this function in equation (10), we obtain

$$\frac{dp_i}{dt} = 1 - r(\Phi(p_i))p_i^2. \tag{21}$$

We now solve this equation for an initial value  $p_i(0) = p$  to obtain  $p_i = p_i(t; p)$ . Then  $F_i(t) = \Phi(p_i(t; p))$ . Using that  $F_i$  is a function of  $i - ct/\delta$  in the wavefront profile, we have  $F_{i-1}(t = 0) = F_i(t = -\delta/c) = \Phi(p_i(-\delta/c; p))$ . The equation

$$\mathcal{F}(\Xi(F_0) - 1) = \Phi\left(p_i\left(-\frac{\delta}{c}; p\right)\right) \tag{22}$$

determines  $F_0$  as a function of  $p$  with  $F_0 - \mathcal{F}(\Xi(F_0) - 1) \neq 0$ .

Once we have determined  $p_i$  as a function of  $F_i$  by means of equation (20), we can solve the fast equation

$$\begin{aligned} -c \frac{dF_i}{d\xi} + \left(p_i(F_i) + \frac{F_i - F_{i-1}}{v}\right)v(F_i) \\ - D(F_i) \left(p_{i+1}(F_{i+1}) - p_i(F_i) + \frac{F_{i+1} + F_{i-1} - 2F_i}{v}\right) = J \end{aligned} \tag{23}$$

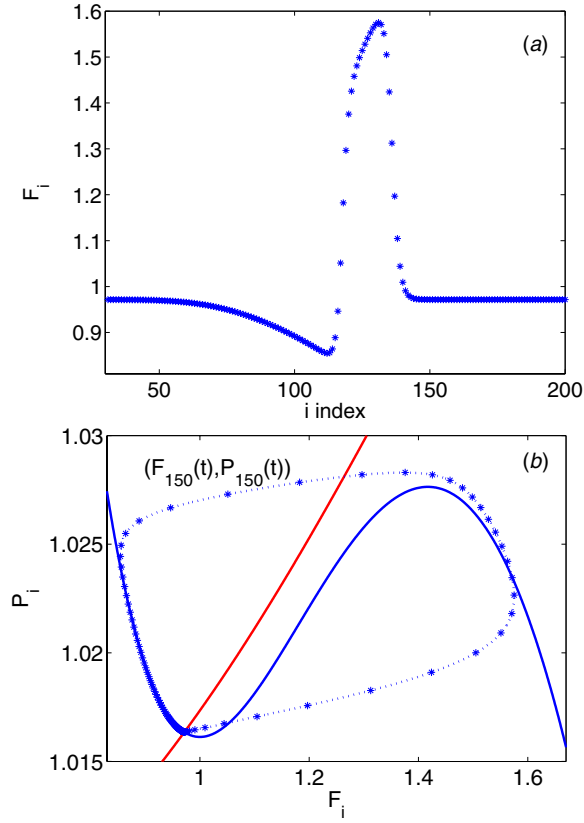
with  $F_i = F(\xi)$ ,  $F_{i\pm 1} = F(\xi \pm 1)$ , and boundary conditions (for  $c > 0$ )

$$F_i(-\infty) = F(+\infty) = F^{(3)}(p'), \quad \text{and} \quad F_i(+\infty) = F(-\infty) = F^{(1)}(p), \tag{24}$$

for the IFs and

$$F_i(-\infty) = F(+\infty) = F^{(1)}(p'), \quad \text{and} \quad F_i(+\infty) = F(-\infty) = F^{(3)}(p), \tag{25}$$

for the DFs. In equation (24), the value  $p' \neq p$  is determined by solving equations (20) and (23), until the first branch of  $J/v(F)$  is reached. Similarly, for a DF,  $p'$  in equation (25) is found by solving equations (20) and (23), until the third branch of  $J/v(F)$  is reached. The front velocity is now a function of  $\delta$ , and figure 5 shows that it is a much better approximation to the numerically calculated front velocity than that given by the leading order theory. In practice, it is easier to calculate directly the finite differences  $\mp(F_i - F_{i\pm 1})$  as functions of  $F_i$ .



**Figure 6.** (a) Numerically obtained field profile of a pulse moving with positive velocity for  $J = 1.013$ ,  $v = 8.44565$ ,  $\delta = 3.7288 \times 10^{-3}$ . (b) Phase plane showing the nullclines and the motion of the 150th QW as the pulse traverses it. The laser intensity is  $120.5 \text{ kW cm}^{-2}$ .

#### 4. Pulses moving downstream in an excitable SL

As we see in figure 6(a), a pulse moving downstream with *positive* velocity consists of regions of smooth field variation on the time scale  $t$ , separated by sharp interfaces in which  $F_i$  varies rapidly on the time scale  $t/\delta$ . To find an asymptotic approximation to the pulse profile, we first use the leading order description of its component wave fronts, according to which  $p_i$  is a constant independent of  $i$  inside the wave front. We can now discuss different regions in the asymptotic description of a pulse, recalling that the field profile is the mirror image of the motion of a QW,  $F_i(t) = F(i - ct/\delta)$ .

##### 4.1. Only one critical point on a stable branch of $J/v(F)$ (leading order theory)

First of all, we describe the pulses for values of  $J$  and  $v$  such that there is one critical point  $(F_*, p_*)$  located on the first branch of  $J/v(F)$ . There are no other critical points or, if they exist, they are located on the second branch of  $J/v(F)$ . Similar results are obtained if the critical point is on the third branch of  $J/v(F)$ .

- The region of smooth variation of  $F$  in front of the pulse is described by equations (9) and (10). In this region,  $F_i = F^{(1)}(p_i)$  so that

$$\frac{dp_i}{dt} = 1 - r(F^{(1)}(p_i))p_i^2,$$

and initial data evolve exponentially fast toward equilibrium,  $F_i = F_*$ ,  $p_i = p_*$ .

- For the pulse leading edge, let  $p(t)$  be the value of  $p_i$  at the last point of the region in front of the pulse. Eventually,  $p \rightarrow p_*$ . At the leading edge,  $F_i(t) = F(i - ct/\delta)$  is a DF moving toward the right with velocity  $C = c(J, v, p)/\delta$  measured in QWs per unit time  $t$ . The DF satisfies equation (11) with the boundary conditions in equation (13). It is convenient to call  $c_-(p) = c(J, v, p)$ . Eventually,  $C \sim c_-(p_*)/\delta$ , and  $F_i$  decreases from  $F_i = F_{\max}$  to  $F_i = F_*$  across the leading edge of the pulse.
- For the region between fronts,  $F_i = F^{(3)}(p_i)$  and

$$\frac{dp_i}{dt} = 1 - r(F^{(3)}(p_i))p_i^2.$$

There is a finite number of points in this region. On its far right,  $p_i = p \rightarrow p_*$ . As we move toward the left,  $p_i$  increases until it reaches a certain value  $P(t)$  corresponding to that in the trailing wave front.

- For the trailing wave front,  $p_i(t) = p(\xi) = P$ , and  $F_i(t) = F(\xi)$  is an IF satisfying equation (11) with the boundary conditions of equation (14). This front moves with velocity  $C = c(J, v, P)/\delta$  measured in QWs per unit time  $t$ . It is convenient to denote  $c_+(P) = c(J, v, P)$ . We indicate how to determine  $P$  below. Clearly, if the pulse moves rigidly, we should have  $c_+(P) = c_-(p_*)$  after a sufficiently long transient period.
- For the pulse tail, we again have  $F_i = F^{(1)}(p_i)$  and  $dp_i/dt = 1 - r(F^{(1)}(p_i))p_i^2$ . Sufficiently far to the left,  $p_i = p_*$ ,  $F_i = F_*$ .

The number of QWs between wave fronts of the pulse can be calculated as follows [16]. Let  $\tau$  be the delay between fronts, i.e. the time elapsed from the moment, at which the leading front traverses the QW  $i = I$ , to the moment, when the trailing front is at  $i = I$ . Clearly,

$$\tau = \int_{p(t-\tau)}^{P(t)} \frac{dp}{1 - r(F^{(3)}(p))p^2}. \quad (26)$$

The number of QWs between fronts,  $m(t)$ , is

$$m = \frac{1}{\delta} \int_{t-\tau}^t c_-(p(t)) dt. \quad (27)$$

However, the separation between fronts satisfies the equation

$$\frac{dm}{dt} = \frac{c_-(p(t)) - c_+(P(t))}{\delta}. \quad (28)$$

The three equations (26)–(28) can be solved to obtain the three unknowns  $\tau$ ,  $m$  and  $P(t)$ . The function  $p(t)$  is determined by solving equation (10) with  $F_i = F^{(1)}(p_i)$  in the region to the left of the leading front.

After a transient period,  $p(t) \rightarrow p_*$  and  $P(t) \rightarrow P$  (a constant value) so that we arrive at the simpler expressions

$$\tau = \int_{p_*}^P \frac{dp}{1 - r(F^{(3)}(p))p^2}, \quad \text{and} \quad (29)$$

$$\frac{dm}{dt} = \frac{c_-(p_*) - c_+(P)}{\delta} \quad (30)$$

instead of equations (26) and (28), respectively. The number of points at the pulse top is now

$$m = \frac{c_-(p_*)\tau}{\delta} = \frac{c_-(p_*)}{\delta} \int_{p_*}^P \frac{dp}{1 - r(F^{(3)}(p))p^2}. \quad (31)$$

This equation yields  $P$  as a function of  $m$ . Then, equation (30) becomes an autonomous differential equation for  $m$  that has a stable constant solution at  $m = m^*$  such that  $c_-(p_*) = c_+(P(m^*))$ : At  $m = m^*$ , the right-hand side of equation (30) has a slope  $-[1 - r(F^{(3)}(J/P))P^2]c'_+(P)/c_-(p_*) < 0$ .

Recapitulating, for appropriate initial conditions, leading and trailing fronts of a pulse evolve until  $m$  reaches its stable value at which  $c_-(p_*) = c_+(P(m^*))$  and equation (31) holds. To compute  $m^*$ , we first determine  $P^* = P(m^*)$  by using  $c_-(p_*) = c_+(P(m^*))$ . Then, we calculate  $\tau = \tau^*$  (which does not depend on  $\delta$ !) from equation (29) and  $m^* = c_-(p_*)\tau^*/\delta$ . Our construction breaks down if the number of QWs between fronts falls below 1. This yields an upper bound for the critical value of  $\delta$  above which pulse propagation fails:  $\delta_c \sim c_-(p_*)\tau^*$ . Pulse propagation may also fail if the leading front becomes pinned for a current density on the interval  $(J_{c1}, J_{c2})$  as mentioned in the previous section [1, 17–19].

To calculate the asymptotic length of the pulse tail, we cannot use equation (29) with  $F^{(1)}$  replacing  $F^{(3)}$  in that formula, because the resulting time becomes infinite. However, we can calculate the time it takes for a solution  $p(t)$  of equation (21) with  $\Phi(p) = F^{(1)}(p)$  and  $p(0) = P$  to reach a neighborhood of  $p_*$ . From that equation, we obtain

$$t = \int_p^P \frac{dp}{r(F^{(1)}(p))p^2 - 1} \sim \int_{p_*}^P \left[ \frac{1}{r(F^{(1)}(p))p^2 - 1} - \frac{1}{(rp^2)'_*(p - p_*)} \right] dp + \frac{1}{(rp^2)'_*} \ln \left( \frac{P - p_*}{p - p_*} \right),$$

with  $(rp^2)'_* = d[r(F^{(1)}(p))p^2]/dp|_{p=p_*} > 0$ , and therefore

$$p(t) - p_* \sim (P - p_*) e^{-(rp^2)'_*(t-T)}, \quad T = \int_{p_*}^P \left[ \frac{1}{r(F^{(1)}(p))p^2 - 1} - \frac{1}{(rp^2)'_*(p - p_*)} \right] dp, \quad (32)$$

for long times such that  $p(t)$  is sufficiently close to  $p_*$ . The time needed for  $p(t)$  to go from  $P$  to  $p_* + (P - p_*)/e$  is then  $T_* = T + 1/(rp^2)'_*$ . The tail length is approximately given by  $M = c_-(p_*)T_*/\delta$ .

#### 4.2. Only one critical point on a stable branch of $J/v(F)$ (corrected theory)

How do we correct this pulse construction using our improved theory of wave fronts?

- The region of smooth variation in front of the pulse is as described above.
- However, we have to use equation (23) instead of equation (11) including the boundary conditions of equation (24) or (25) to construct the leading and trailing wave fronts of the pulse. Let us assume that the pulse moves from left to right. The leading wave front is a DF moving with velocity  $c_-(p)/\delta$  with  $c_-(p) = c(J, v, p, \delta)$  given by equation (23) and the boundary conditions of equation (25). While  $p(t)$  is the value at the initial field on the first branch of  $J/v(F)$ ,  $p'(t)$  is the hole density at the final QW of the DF which is on the third branch of  $J/v(F)$ . The time it takes for a QW to move from  $(F^{(1)}(p), p)$  to  $(F^{(3)}(p'), p')$  is of order  $\delta$ , and it needs to be considered when constructing the pulse.
- In the region between leading and trailing fronts,  $F_i = F^{(3)}(p_i)$ . On its far right,  $p_i = p' \rightarrow p'_*$ , where we call  $p'_*$  the value of  $p'$  corresponding to  $p = p_*$ . As we move toward the left,  $p_i$  increases until it reaches a certain value  $P(t)$  corresponding to that in the trailing wave front.

- The trailing wave front is an IF moving with velocity  $c_+(P)/\delta$ , with  $c_+(P) = c(J, v, P, \delta)$  given by equation (23) and the boundary conditions of equation (24). The hole densities at the initial and final QWs of the IF are  $P$  and  $P'$ , respectively. The corresponding fields are  $F^{(3)}(P)$  and  $F^{(1)}(P')$ , respectively. Again the time it takes for a QW to move from  $(F^{(3)}(P), P)$  to  $(F^{(1)}(P'), P')$  is of order  $\delta$  and will be included in our calculations to order  $\delta$ .
- The pulse tail is as described above except that its first QW has a hole density  $P'$  instead of  $P$ .

Equations (26)–(28) become

$$\tau = \int_{p'(t-\tau)}^{P(t)} \frac{dp}{1 - r(F^{(3)}(p))p^2}, \quad (33)$$

$$m = \frac{1}{\delta} \int_{t-\tau}^t c_-(p(t)) dt, \quad (34)$$

$$\frac{dm}{dt} = \frac{c_-(p'(t)) - c_+(P(t))}{\delta}. \quad (35)$$

After the transient period, these equations become equations (29)–(31) with  $p'$  (now time independent) instead of  $p_*$ . The rest of the considerations made above apply except that now  $\tau^*$  depends on  $\delta$  because  $p'_*$  does.

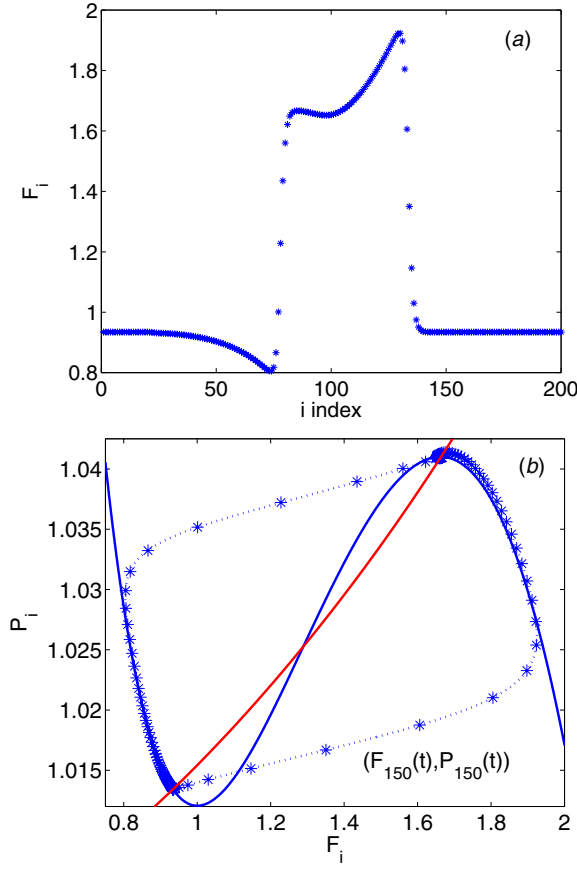
#### 4.3. Two critical points on the stable branches of $J/v(F)$

In the case illustrated in figure 7, there is one critical point on each of the three branches of  $J/v(F)$ . Let  $(F_*, p_*)$  and  $(F^*, p^*)$  be the critical points on the first and third branches of  $J/v(F)$ , respectively. This case is very similar to that described before for the case of a sole critical point on the first branch. However, now  $c_-(p_*) \neq c_+(p^*)$  except for particular values of  $J$ . Therefore, these pulses do not move rigidly in general: they will shrink and disappear or grow indefinitely. Regions 1 to 3 of the pulse in figure 7(a) are identical to those of the pulse with only one critical point, except that now  $p \rightarrow p_*$  and  $P \rightarrow p^*$ , and  $m$  either decays to zero or it grows indefinitely.

### 5. Wave trains moving downstream in a dc-current-biased photoexcited SL

For the spatially discrete FHN system, wave trains were constructed by Carpio using matched asymptotic expansions [15]. A similar construction could be carried out using our improved theory of wave fronts. A wave train consists of a periodic profile  $F(\xi)$ ,  $p(\xi)$ ,  $\xi = i - ct/\delta$ , with period  $L$  and velocity  $c$ . Figure 8(a) gives the corresponding field profile: a first smaller pulse triggers a periodic succession of equal pulses, which become the wave train. Figure 8(b) shows the passage of a wave train through a QW: starting at an unstable stationary state, trajectories in the phase plane evolve toward a stable limit cycle. The wave train profiles can be reconstructed from a time periodic solution  $F_i(t) = F(i - ct/\delta)$ ,  $p_i(t) = p(i - ct/\delta)$ , with time period  $T = L\delta/c$  and velocity  $c$ . The spatial structure of the wave train at each fixed time  $t$  is given by  $F_i(t) = F(i - ct/\delta)$  and  $p_i(t) = p(i - ct/\delta)$ . The points contained in a period satisfy  $0 \leq i - ct/\delta \leq L$ , that is,  $ct/\delta \leq i \leq L + ct/\delta$ . As time grows, the discrete points *travel* along the continuous wave profile and are transferred from one period to the next. The number of integers  $i$  one can fit in an interval of length  $L$  is the integer part of  $L$ .

Assuming a positive velocity, there are four stages in one time period of the wave trains  $(F_i(T, \delta), p_i(T, \delta))$ :



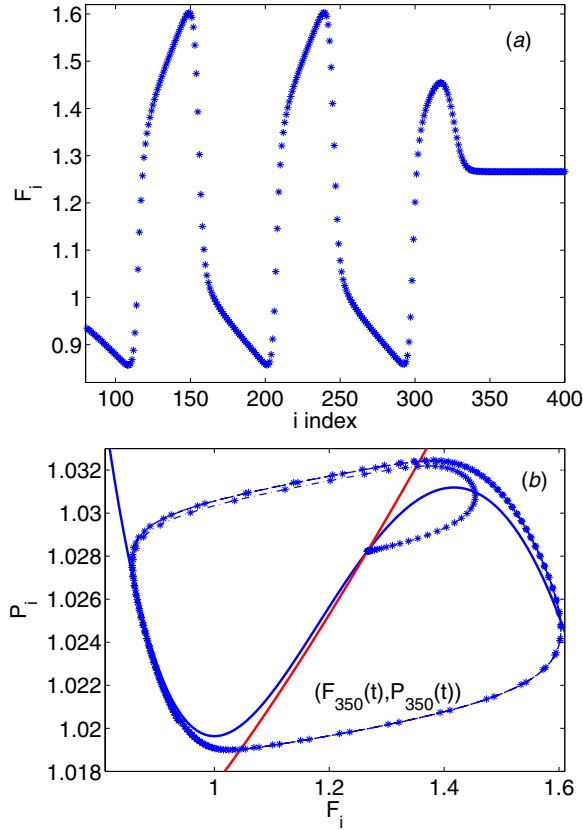
**Figure 7.** (a) Numerically obtained field profile of a pulse moving with positive velocity when there are three critical points in the phase plane. (b) Phase plane showing the nullclines and the motion of the 150th QW as the pulse traverses it.  $J = 1.009$ . The photoexcitation intensity is  $120.5 \text{ kW cm}^{-2}$ .

- For leading-edge DFs given by equations (20) and (23) using the boundary conditions of equation (25), the DF velocity is  $c_-(p)/\delta$  with  $c_-(p) = c(J, v, p, \delta)$ , where  $p(t)$  is the value at the initial field on the first branch of  $J/v(F)$  and  $p'(t)$  is the hole density at the final QW of the DF, whose corresponding field is on the third branch of  $J/v(F)$ . The time it takes for a QW to move from  $(F^{(1)}(p), p)$  to  $(F^{(3)}(p'), p')$  is of order  $\delta$ , and we should consider it when constructing the train.
- In the peak region between leading and trailing fronts,  $F_i = F^{(3)}(p_i)$ . On its far right,  $p_i = p'$ . As we move toward the left,  $p_i$  increases until it reaches a certain value  $P(t)$  corresponding to that in the trailing wave front.  $P(t)$  will be calculated later. The duration of this stage is

$$T_p = \int_{p'}^P \frac{dp}{1 - r(F^{(3)}(p))p^2}. \quad (36)$$

Note that  $T_p$  may become infinite if there is a fixed point  $(F^*, p^*)$  on the third branch of  $J/v(F)$ . In such a case, we may have wave trains only if  $p < p^*$ .

- The trailing wave front is an IF moving with velocity  $c_+(P)/\delta$ , with  $c_+(P) = c(J, v, P, \delta)$  given by equation (22) and the boundary conditions of equation (24). The hole densities at



**Figure 8.** (a) Numerically obtained field profile of a pulse moving with positive velocity followed by a wave train when there is only one critical point in the phase plane. (b) Phase plane showing the nullclines and the motion of the 350th QW as the pulse traverses it for  $J = 1.0165$ . The photoexcitation intensity corresponds to  $120.5 \text{ kW cm}^{-2}$ .

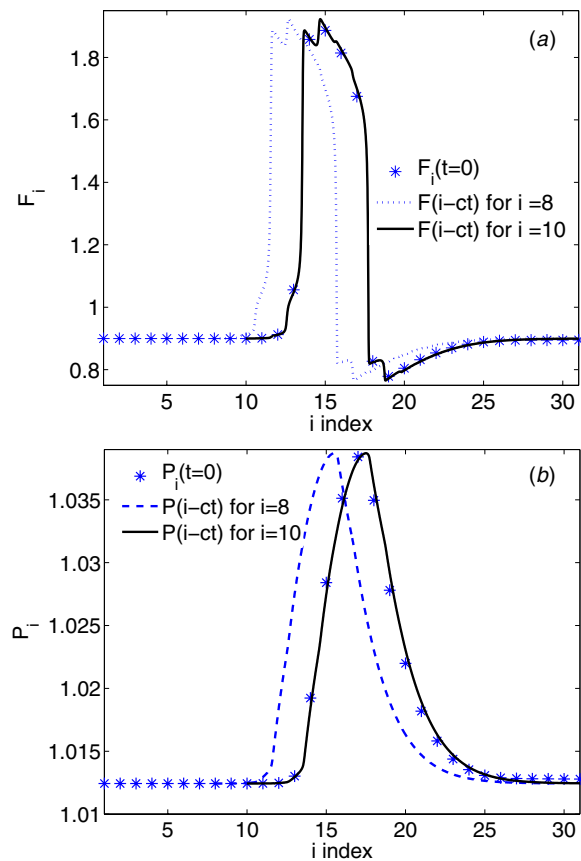
the initial and final QWs of the IF are  $P$  and  $P'$ , respectively, and the corresponding fields are  $F^{(3)}(P)$  and  $F^{(1)}(P')$ , respectively. Again, the time it takes for a QW to move from  $(F^{(3)}(P), P)$  to  $(F^{(1)}(P'), P')$  is of order  $\delta$  and will be ignored. For the wave train to move rigidly, we must have  $c_-(p) = c_+(P) = c$ . This condition gives  $P$  as a function of  $p$ .

- In the tail of the wave train,  $F_i = F^{(1)}(p_i)$ . On the far right of the tail region,  $p_i = P'$  and  $p_i$  decreases until it reaches the value  $p$ . The duration of this stage is

$$T_t = \int_{p'}^p \frac{dp}{1 - r(F^{(1)}(p))p^2}. \quad (37)$$

Note that  $T_t$  may become infinite if there is a fixed point  $(F_*, p_*)$  on the first branch of  $J/v(F)$ . In such a case, we may have wave trains only if  $p > p_*$ .

The previous construction of the wave train gives its velocity and period  $T \sim T_p + T_t$  as functions of the parameter  $p$ . The spatial period  $L$  is the integer part of  $cT/\delta$ . The number of QWs in the peak (respectively the tail) region is the integer part of  $c_-(p)T_p/\delta$  (respectively  $c_-(p)T_t/\delta$ ). Our construction clearly fails if the number of QWs in the peak region is smaller than 1, i.e. if  $c_-(p)T_p < \delta$ . Thus,  $\delta$  has to be larger than  $c_-(p)T_p$ .



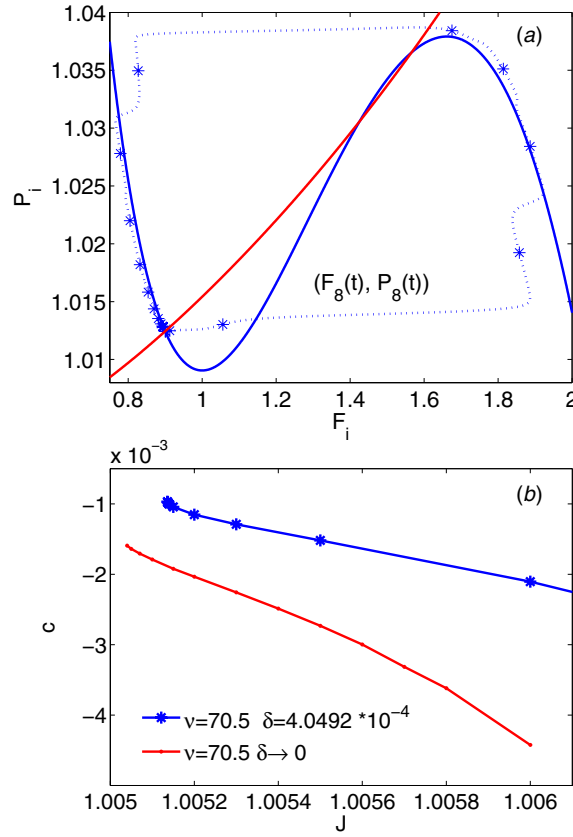
**Figure 9.** (a) Numerically obtained field profile of a pulse moving with negative velocity for  $J = 1.009$ ,  $v = 70.5$ ,  $\delta = 4.05 \times 10^{-4}$ . (b) Numerically obtained hole density profile of the same pulse. The laser intensity is  $479.7 \text{ kW cm}^{-2}$ .

### 6. Pulses moving upstream in a dc-current-biased photoexcited SL that behaves as an excitable medium

Numerical simulations of the complete model show pulses moving upstream with a negative velocity, both under dc current bias and under dc voltage bias. Although the field profile of these pulses is quite similar to that of downstream moving pulses (cf figures 6 and 9), there are fundamental differences between them. The velocity of these pulses is much smaller than that of downstream moving pulses, and they cannot be approximated by one IF and one DF plus regions of slow variation of the electric field. In fact, figure 4(b) shows that, contrary to the case of wave fronts moving with positive velocity depicted in figure 4(a), it is not possible for a DF and an IF to move with the same negative velocity at a fixed  $J$ . Thus, our construction of pulses in section 4 cannot describe pulses that move rigidly upstream with negative velocity.

The asymptotic construction of pulses moving rigidly with negative velocity under dc current bias is necessarily different from the case of downstream moving pulses. The rigid upstream motion of pulses is saltatory: although the velocity of the pulse is constant ( $c < 0$ ), there are periods in which the QWs move slowly on the pulse field profile separated by fast





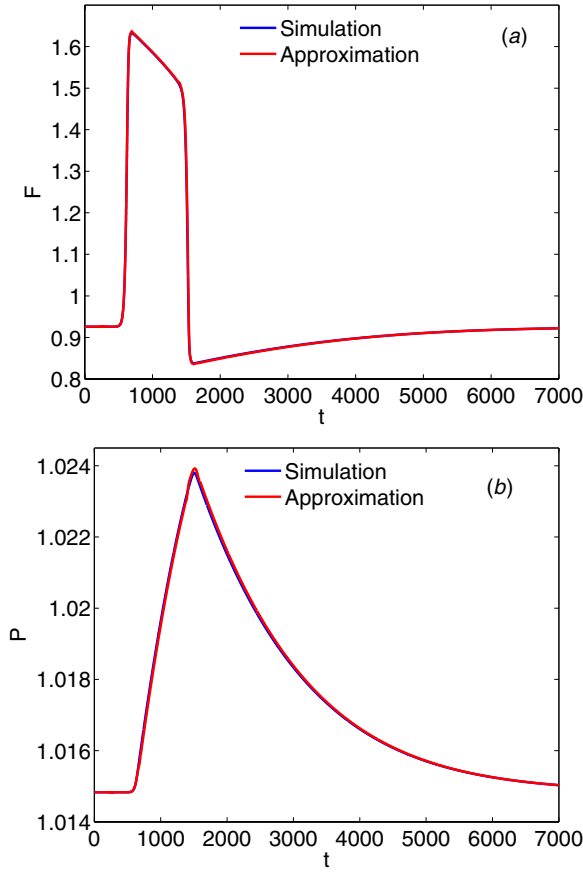
**Figure 10.** (a) Phase plane showing the nullclines and the motion of the 8th QW as the pulse traverses it for the profiles depicted in figure 9. (b) Comparison of the pulse velocity obtained from leading order perturbation theory and that obtained from numerical simulations.

transitions as shown in figure 9(a). Figure 9(b) shows that the hole density changes smoothly even at the fast transitions in the field profile. During the slow periods, the field and hole density at the QWs evolve according to the following equations:

$$\left( p_i + \frac{F_i - F_{i-1}}{v} \right) v(F_i) - \left( p_{i+1} - p_i + \frac{F_{i+1} + F_{i-1} - 2F_i}{v} \right) D(F_i) = J, \quad (38)$$

$$\frac{dp_i}{dt} = 1 - r(F_i) p_i \left( p_i + \frac{F_i - F_{i-1}}{v} \right), \quad (39)$$

which have been obtained by setting  $\delta = 0$  in equations (7)–(8). We have to solve equation (38) for the profile  $\{F_i\}$  in terms of the instantaneous values of the  $\{p_i\}$  and insert the result in equation (39). It turns out that there are several possible solutions corresponding to integer shifts of the pulse profile  $i \rightarrow i + m, m = 0, \pm 1, \dots$ . The implicit function theorem establishes that, starting from an appropriate pulse-like initial condition, it is possible to find  $F_i = F_i(\{p_j\})$ , provided the Jacobian determinant corresponding to equation (38) is not zero. This condition holds until the QWs reach the points of abrupt field change in figure 9(a) or 10(a) (phase



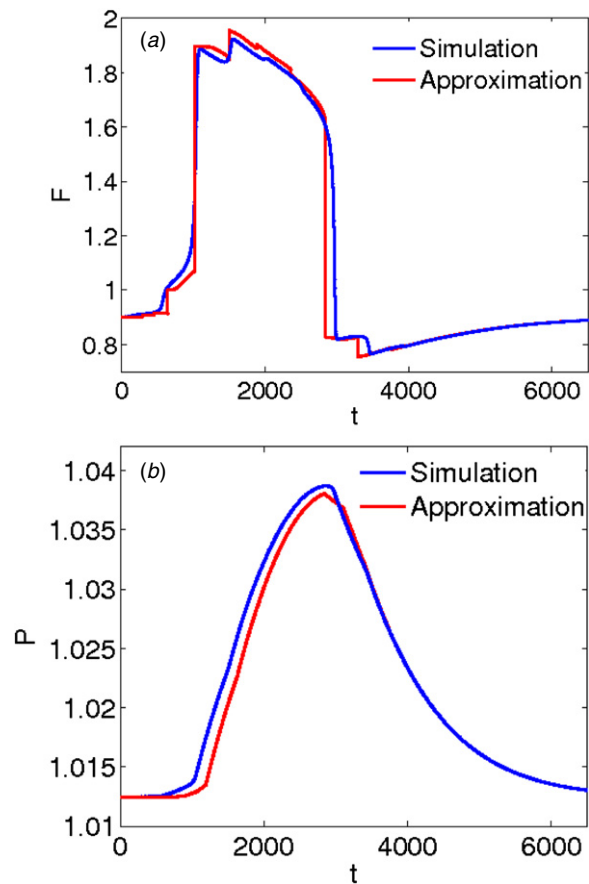
**Figure 11.** (a) Reconstruction of a pulse of the electric field moving with a positive velocity for  $J = 1.009$ ,  $v = 70.5$ ,  $\delta = 4.05 \times 10^{-4}$  as in figure 7. (b) Reconstruction of the corresponding hole density profile.

plane) at times  $t = t_a$ . Then, the Jacobian vanishes, and the field values change according to

$$\frac{dF_i}{d\tau} = J + \left( p_{i+1} - p_i + \frac{F_{i+1} + F_{i-1} - 2F_i}{v} \right) D(F_i) - \left( p_i + \frac{F_i - F_{i-1}}{v} \right) v(F_i), \quad (40)$$

with  $\tau = (t - t_a)/\delta$  and  $\{p_i\}$  frozen at their values at  $t_a$  given by equations (38)–(39). As explained before, as  $\tau \rightarrow -\infty$  the  $\{F_i(\tau)\}$  tends to the solution of equation (38) for  $t = t_a$ , and it tends to the same profile shifted one step to the left:  $i \rightarrow i - 1$  as  $\tau \rightarrow +\infty$ . Then, another slow stage follows. Figure 10(b) shows the velocity of the pulse. It is approximately the inverse time one QW spends in the short interval of  $p$  between the abrupt long jump in  $F$  from the first branch of  $J/v(F)$  to a value below that in the third branch of  $J/v(F)$  and the abrupt short jump in  $F$  to the third branch of  $J/v(F)$ , which occurs for a somewhat higher value of  $p$  as shown in figure 10(a).

Figures 11(a) and (b) compare the field and hole density profiles of the reconstructed pulse (moving with positive velocity) and those obtained by direct numerical solution of the equations. Similarly, figures 12(a) and (b) compare the field and hole density profiles of the reconstructed pulse (moving with negative velocity) and those obtained by direct numerical



**Figure 12.** (a) Reconstruction of a pulse of the electric field moving with a negative velocity for  $J = 1.009$ ,  $\nu = 70.5$ ,  $\delta = 4.05 \times 10^{-4}$ . (b) Reconstruction of the corresponding hole density profile.

solution of the equations. The agreement is quite reasonable and it could be improved by finding a corrected theory of the pulse velocity.

## 7. Conclusions

An undoped, strongly photoexcited, weakly coupled, dc-current-biased SL exhibits a variety of pulse and wavefront solutions. They can be constructed using matched asymptotic expansions that exploit the large separation of time scales (measured by the dimensionless parameter  $\delta$ ) between the carrier dynamics and the evolution of the electric field. On the time scale of the electron and hole densities, the field follows adiabatically the profiles thereof.

For large photoexcitation, the field profile of a pulse typically consists of slowly varying regions separated by sharp wave fronts. As in the case of the FHN model of nerve conduction, an asymptotic reconstruction of the downstream-moving pulse to leading order in  $\delta$  determines its velocity as the value for which the velocities of the leading and trailing fronts are the same. The comparison of this approximate velocity to that obtained by direct solution of the full

model equations is only fair. For a better agreement, we have improved the description of the wave fronts comprising the pulse by including order  $\delta$  corrections. The resulting corrected theory describes the pulses and their velocities much better. Pulses moving upstream the electron flow exhibit saltatory motion: they alternate periods of very small velocity with fast motion during short time intervals. We have reconstructed them using matched asymptotic expansions in the limit of small  $\delta$ , but the resulting theory is quite different from that of downstream-moving pulses.

### Acknowledgments

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